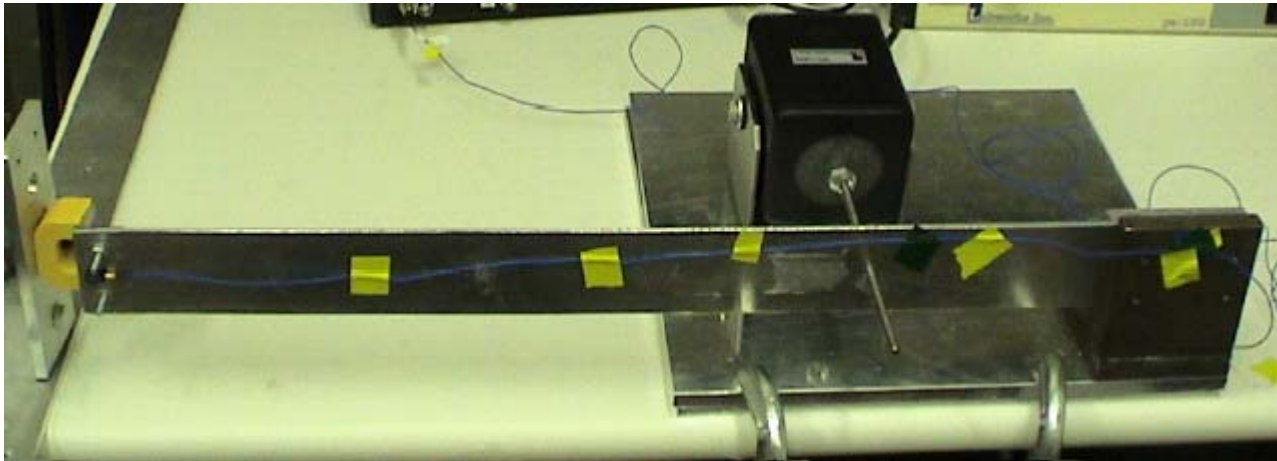
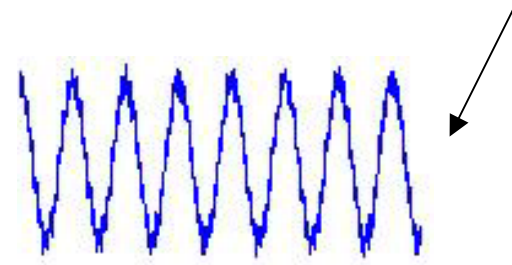
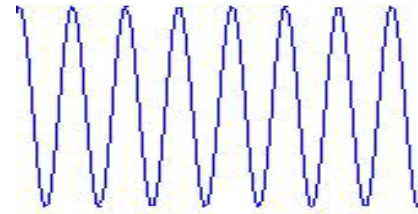

Shaker Control in the Presence of Nonlinearities



Kelly Brinkley, University of Denver
Steve Holman, Montana State University
Kai Yu, Stanford University
Mentor: Matt Bement, LANL Staff

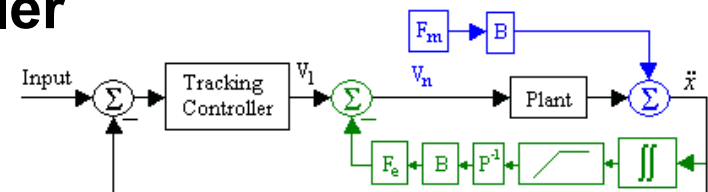
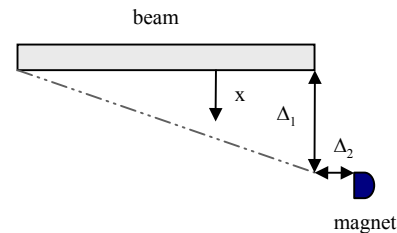
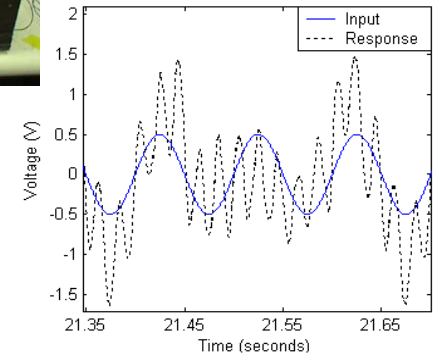
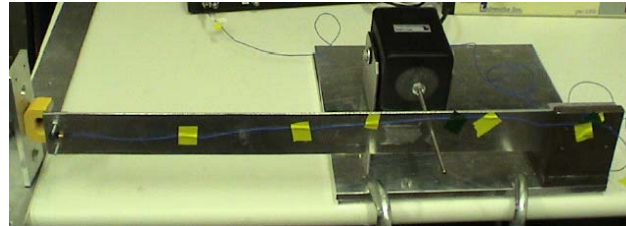
Motivation

- **Shaker control systems are required to remove shaker dynamics and coupling effects**
- **Nonlinearities in a structure or environment can influence input force and measured response in a vibration or accelerated aging tests**
- **Desire to eliminate nonlinear effects using a shaker controller**



Outline

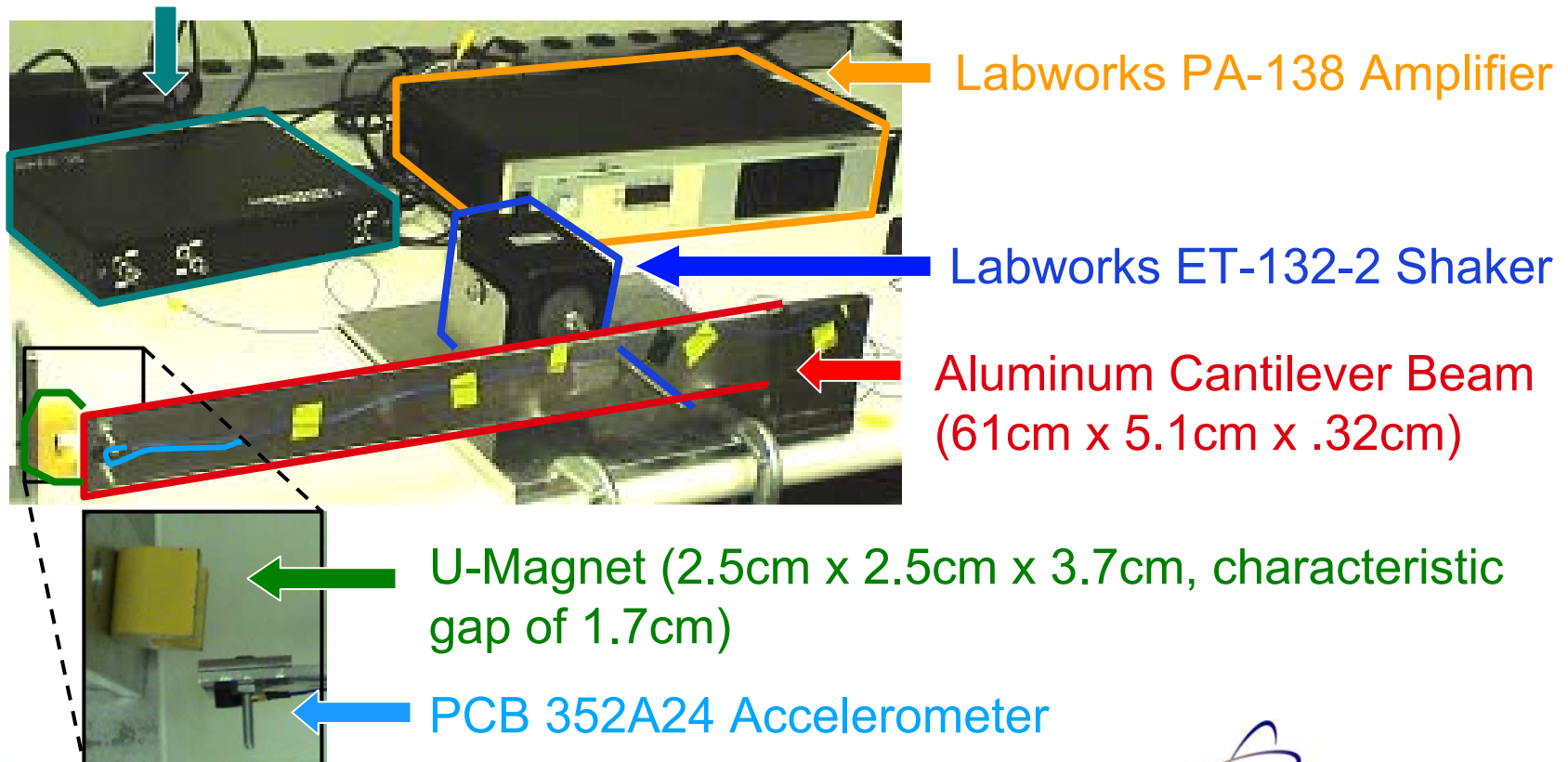
- Experimental Setup
- Nonlinearity
- Modal Parameter Extraction
- Extended Kalman Filter
- Feedback Linearization Controller
- Results



Experimental Setup

PC (not pictured) containing NI PCI 6052E data acquisition card,
XPC real-time OS

National Instruments SC-2345 Signal Conditioner

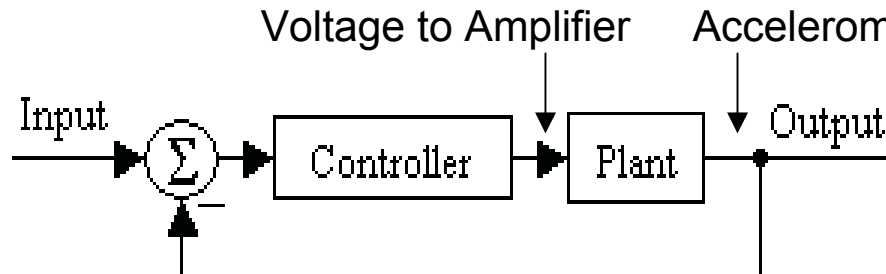


Strategy

- Design a controller to track a 0.5V amplitude, 10 Hz sinusoid without the magnet
- Add magnet and observe tracking with the same controller
- Attempt to remove nonlinearity using feedback linearization controller
 - Use extended Kalman filter to estimate parameters
 - Obtain modal parameters for use in Kalman filter

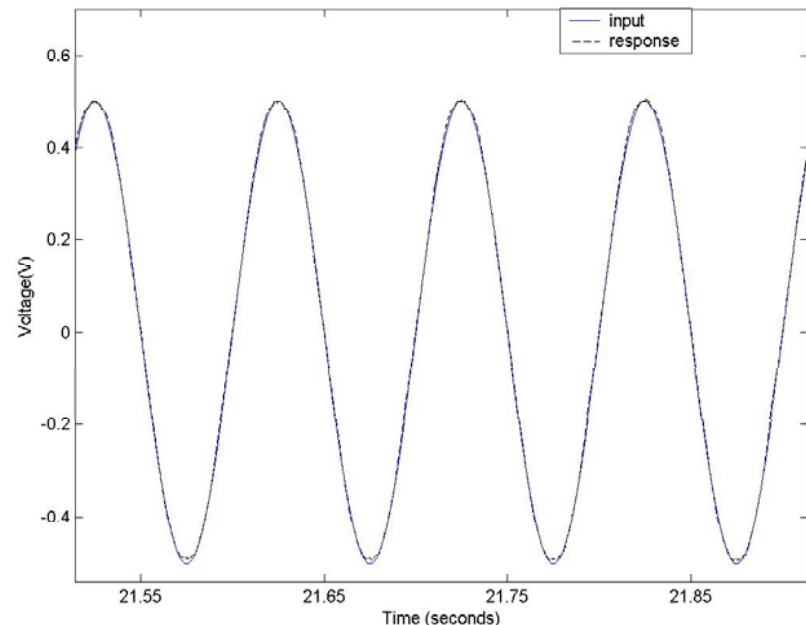


Controls Background



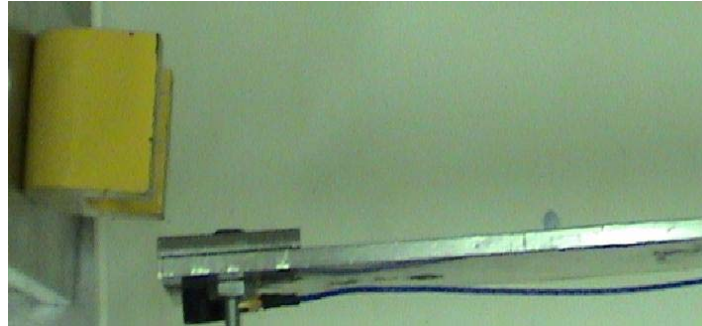
$$T = \frac{P(s)C(s)}{1 + P(s)C(s)}$$

- **Tracking controller makes the output and input waveforms the same**
- **Relatively easy for single frequency, harder for multiple frequencies**

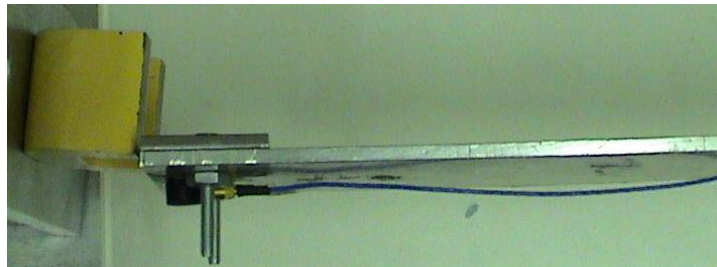


Nonlinearity – Equilibrium Points

- First equilibrium point

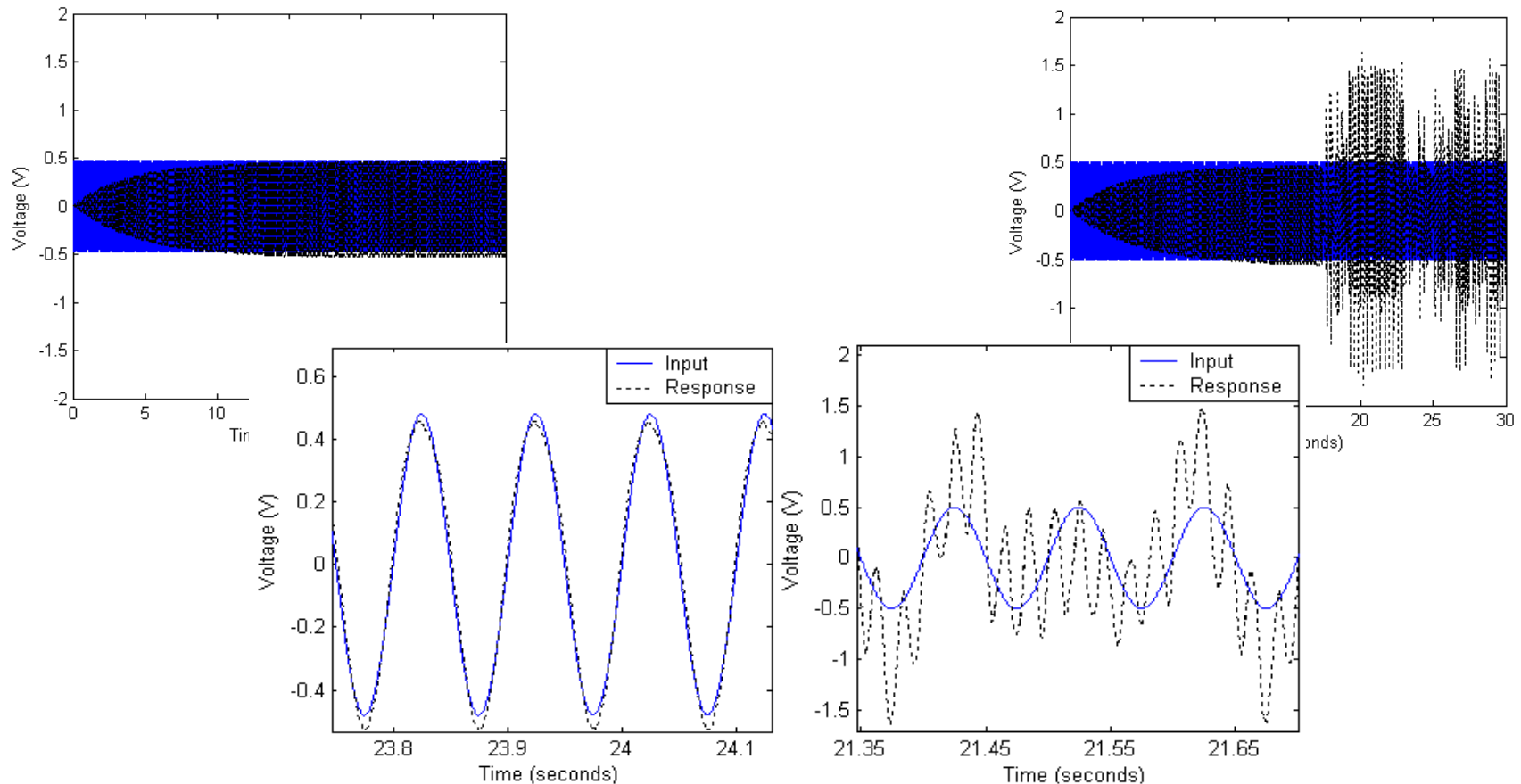


- Second equilibrium point 1.2 cm away



- Magnetic force modeled as: $F = \frac{C}{d^3}$

Nonlinearity - Tracking



- Tracks 0.48V sinusoid, but 0.5V sinusoid reaches a “remote, non-periodic attractor”

Modal Parameter Extraction

- **Impact hammer test on free beam (shaker not attached) and SEREP reduction on FEA data (high fidelity)**
 - SEREP reduced mass and stiffness matrices do not require the original system mass and stiffness matrices.
 - Subsequent reduced mass and stiffness matrices.
- **Generalized inverse of analytical modal vectors**
 - Compare to reduced matrices via generalized inverse – exact same
- **Generalized inverse of experimental modal vectors**
 - Compare – good agreement



Modal Parameter Extraction

- Apply above procedure to true beam (shaker attached) and obtain mass, damping, and stiffness matrices to be used in extended Kalman filter
- Comparison between analytical and experimental through MAC and POC



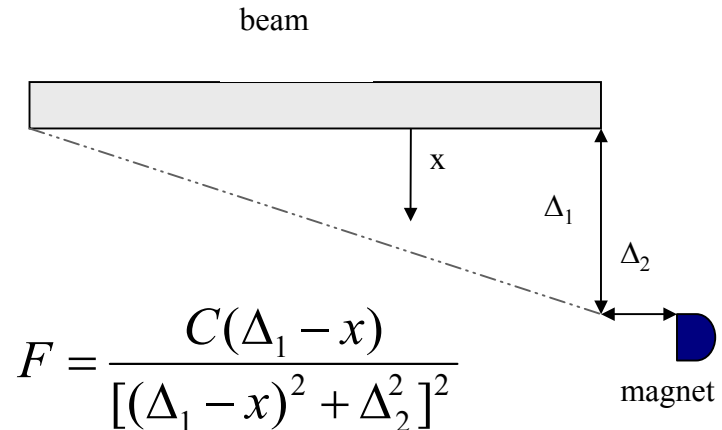
Modal Assurance Criteria with Quill		
0.9947	0.0550	0.0624
0.0314	0.9963	0.2253
0.0785	0.0752	0.9664

Pseudo Orthogonality Check with Quill		
0.9977	-0.0625	0.0243
-0.0059	-0.9978	-0.0664
-0.1004	0.1810	-0.9783

Extended Kalman Filter

- **Purpose**

- Estimate parameters of the magnetic force: C , Δ_1 , and Δ_2



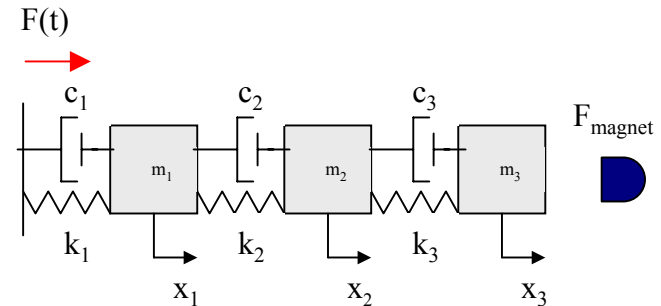
- **Method**

- Extended Kalman Filter (EKF) is a predictor/corrector technique
- First estimates the state and error covariance
- Updates estimates using the Kalman gain

Extended Kalman Filter: Implementation

- Magnetic force
$$F = \frac{C(\Delta_1 - x_3)}{[(\Delta_1 - x_3)^2 + \Delta_2^2]^2}$$

- Assume a 3 degree of freedom model



- Verify convergence in the model with simulations
- Incorporate experimental displacement and modal parameters into the filter
- Verify filter predictions by determining equilibrium points

Results: Extended Kalman Filter

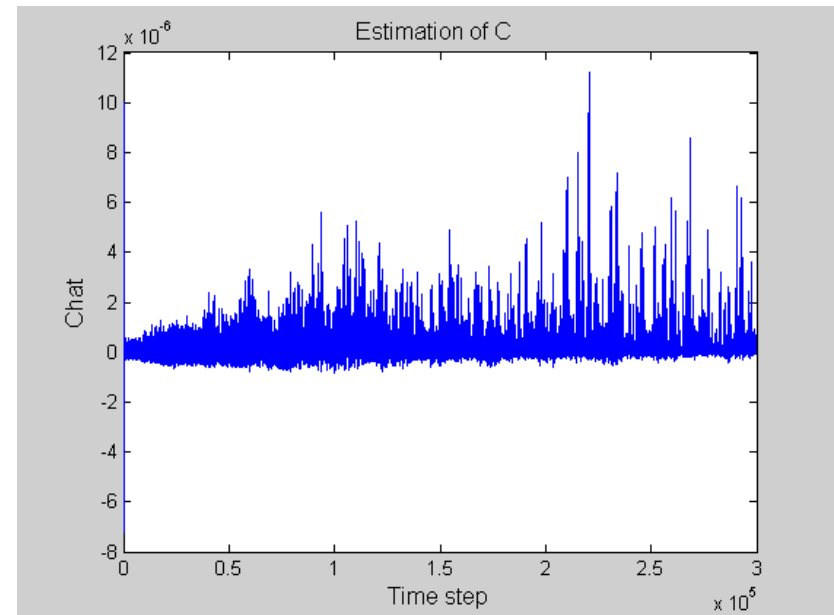
- **Simulated**

Converges for C , Δ_1 , and Δ_2

- Initial estimates must be within $\pm 50\%$ of actual parameter values

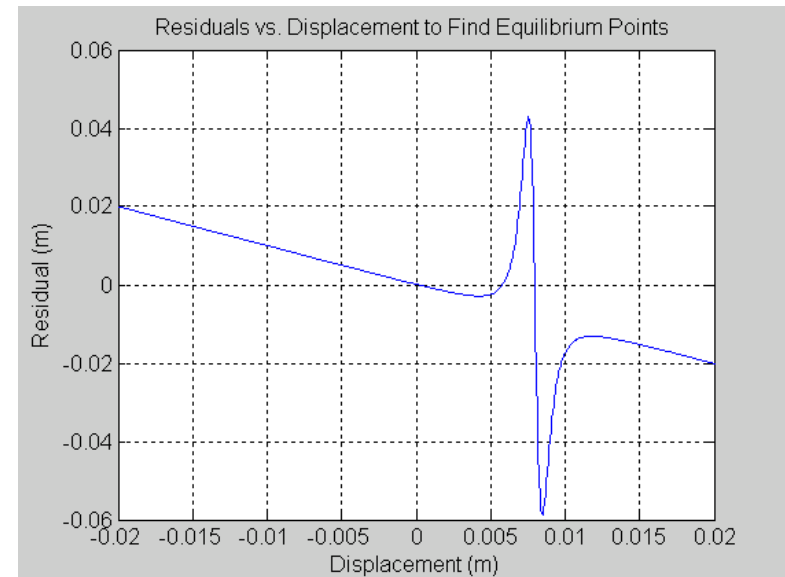
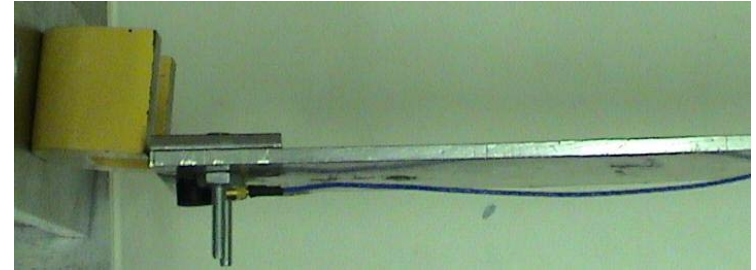
- **Experimental**

- C oscillates in the range of $\pm 10^{-5} \text{ N}\cdot\text{m}^3$
- Δ_1 and Δ_2 do not converge, but stay in the same order of magnitude

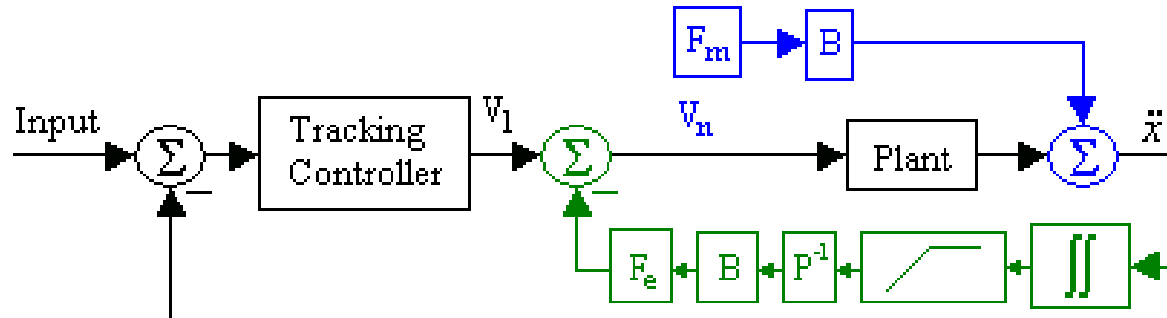


Results: Model Verification

- **Equilibrium Points**
 - For $C = 1.05e-7$, $\Delta_1 = 0.0082\text{m}$, and $\Delta_2 = 0.0008\text{m}$, only one equilibrium point at 0.0080m
 - Decrease C to $1e-8$ to find three points at 0.00016m , 0.0058m , and 0.0080m



Feedback Linearization Controller



Acceleration without Magnet

$$\ddot{x} = P v_l$$

Acceleration with Magnet

$$\ddot{x} = P V_n + B F_m(x)$$

Feedback Linearization Controller

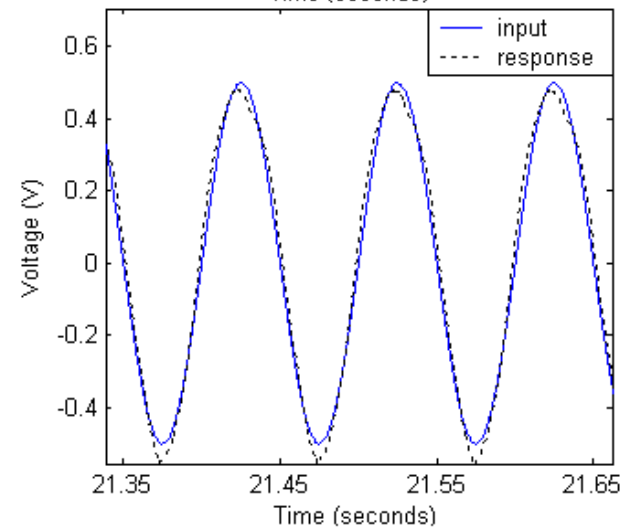
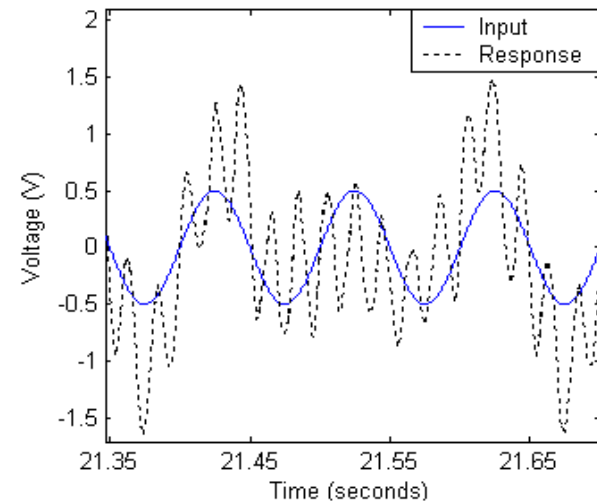
$$V_n = v_l - P^{-1} B F_e(x)$$

Resultant Acceleration

$$\ddot{x} = P v_l$$

Results: Feedback Linearization Controller

- Tracking significantly improved at 0.5V amplitude sinusoid
- Controller did not adversely affect tracking of lower amplitudes
- At higher amplitudes, required voltage exceeded capabilities of D/A channel



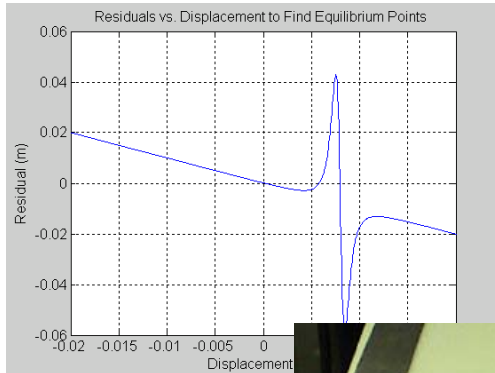
Summary

- **We compensated for the nonlinearity**
- **Extended Kalman filter and equilibrium point check provided acceptable starting point for feedback linearization controller**
- **Recommendations for future research:**
 - Apply technique to a more complex structure
 - Apply technique to a less well-defined nonlinearity
 - Create control to track over frequency range and test feedback linearization controller

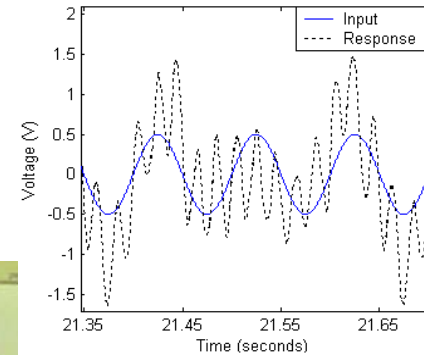
Acknowledgements

- **The completion of this project is largely due to the contribution and help from the following:**
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 - Dr. Peter Avitabile, for his help with data reduction, correlation, system matrix estimation and software
 - Dr. Charles Farrar, for enabling this project to exist by hosting and managing the Dynamics Summer School
 - Department of Energy and the ESA Division, for providing funding for the Dynamics Summer School
 - Vibrant Technologies
 - The Mathworks, Inc.
 - Dynamic Design Solutions
 - Hibbitt, Karlsson, and Sorensen, Inc.

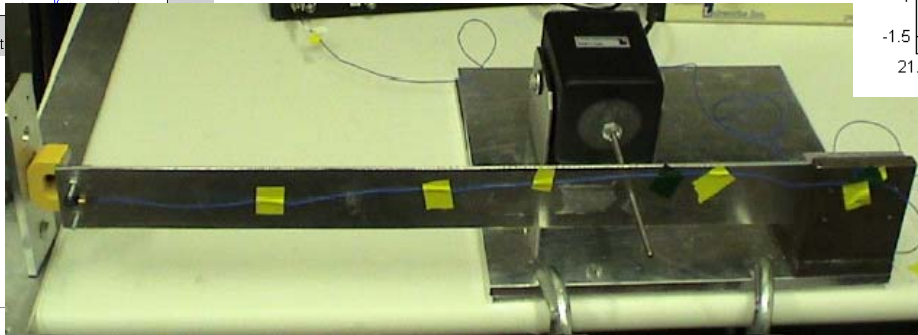
Questions and Comments



Experimental Setup



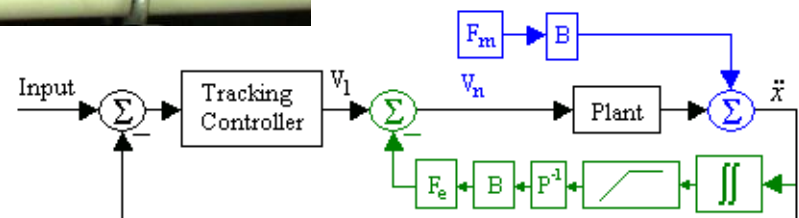
Extended Kalman Filter



Nonlinearity



Modal Parameter Extraction



Feedback Linearization Controller